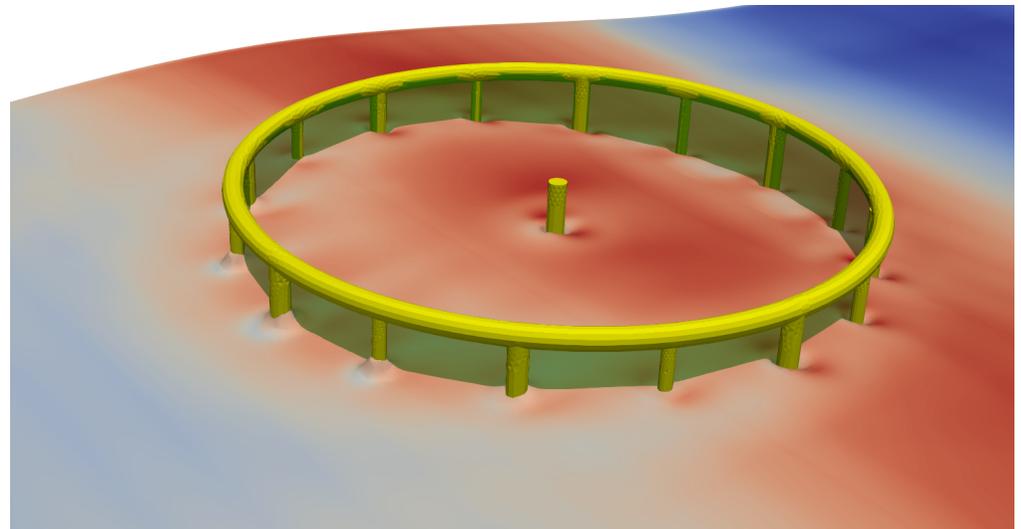


A CFD-Based Numerical Framework for Modelling Open Ocean Aquaculture Structures

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Today's Aquaculture Structures

- mostly inside fjords
- hydrodynamic loading: currents
- protected against large waves
 - mostly $H_{s,max} < 1$ m
 - very few places with $H_s > 1.5$ m
- traffic light system for salmon lice
- higher environmental impact on closed water systems



Ambitious Goals

- increased production
- larger devices
- exposed area: $H_s = 5$ m, $H_s = 16$ m
- exposed for large waves and extreme weather
- outside the traffic light system for salmon lice
- reduced environmental impact in open ocean
- challenging: fish escape & fish mortality



kilde: salmar.no

Project Objectives



Traditional aquaculture in fjords



Open ocean structures

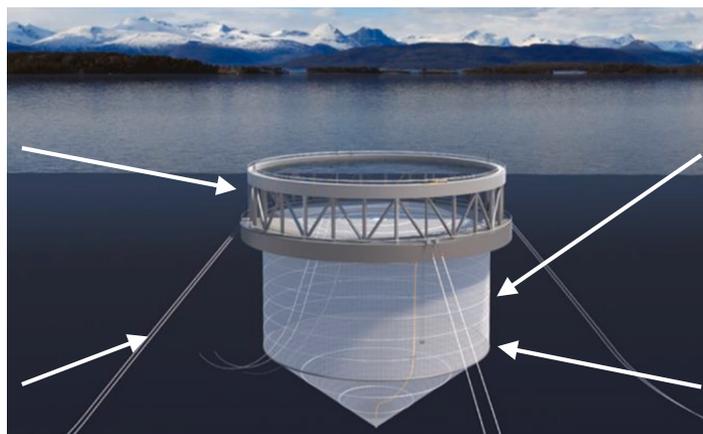


Challenges

- Enable the investigation of offshore aquaculture structures in the ocean
 - Complex FSI
 - Including flexible structures
- Computational Fluid Dynamics
 - Inside into flow pattern around and in the cages
 - Accurate force calculations in severe weather conditions
- Tasks:
 - Developing suitable mooring model
 - Developing suitable net model
 - Modelling the fluid-structure interaction in CFD solver

Rigid-body FSI solver

Mooring dynamics



Fluid-net coupling

Net dynamics

REEF3D::CFD

- Solves:

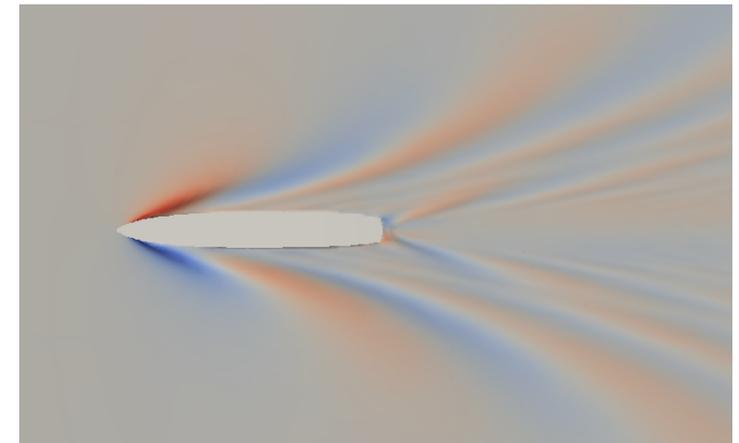
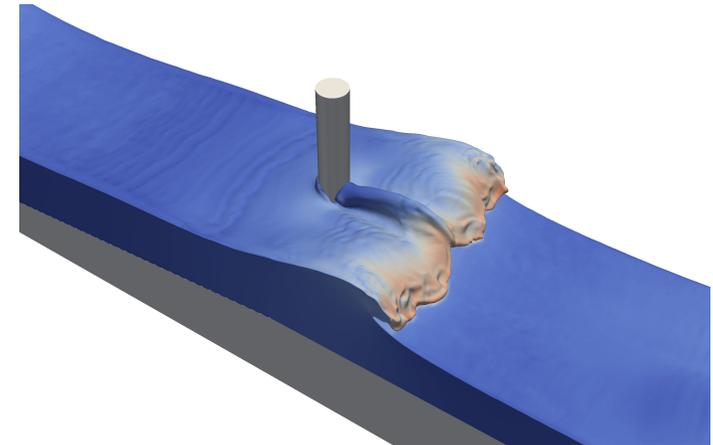
- Full 3D Navier-Stokes Equations
- Free Surface: Two-Phase Flow - Water & Air

- Focus on:

- Free Surface Flows
- Wave Hydrodynamics
- Floating Structures
- Open Channel Flow
- Sediment Transport

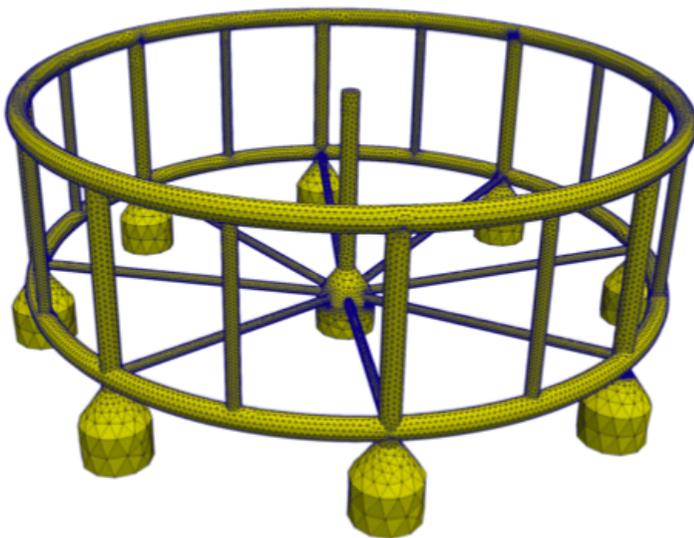
- The Code

- part of the REEF3D hydrodynamic framework
- C++ (modular & extensible)
- Parallel Computing / HPC
- Open-Source: <https://github.com/REEF3D>
- Developed at the Department of Civil and Environmental Engineering, NTNU Trondheim
- More info at: www.reef3d.com
- CFD Online Forum: <https://www.cfd-online.com/Forums/reef3d/>

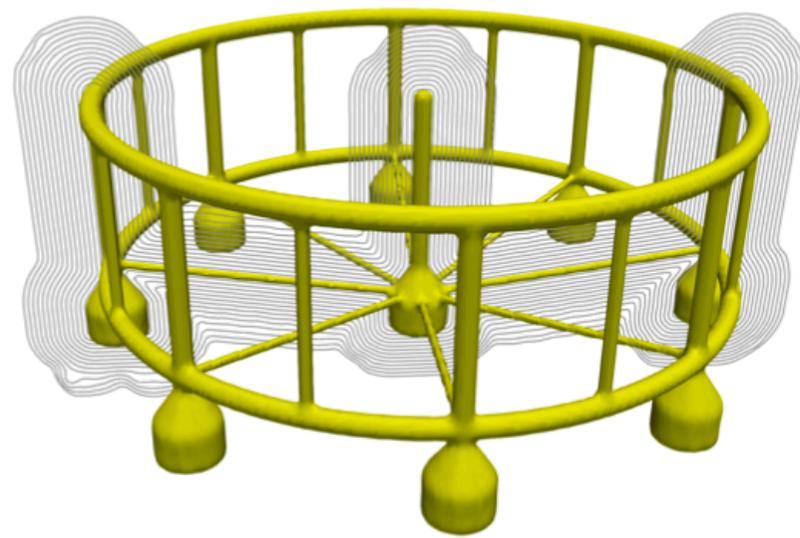


Modelling the Fluid-Structure Interaction

- Direct forcing immersed boundary method
 - Rigid body dynamics described by Euler parameters
 - Weak coupling
 - Implicit boundary conditions enforced with forcing term



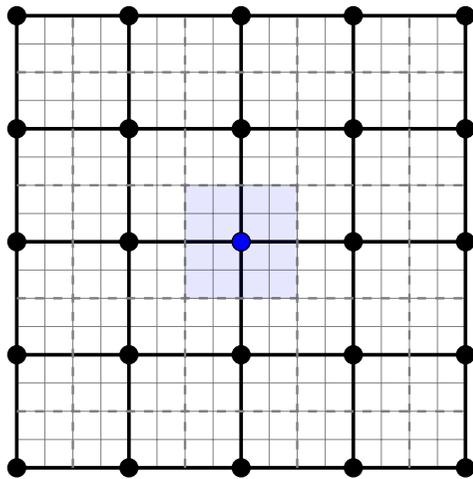
(a) Original STL representation.



(b) Level set representation indicated by grey contour lines in x-z plane. Yellow surface shows $\Phi_s = 0$.

Net Model

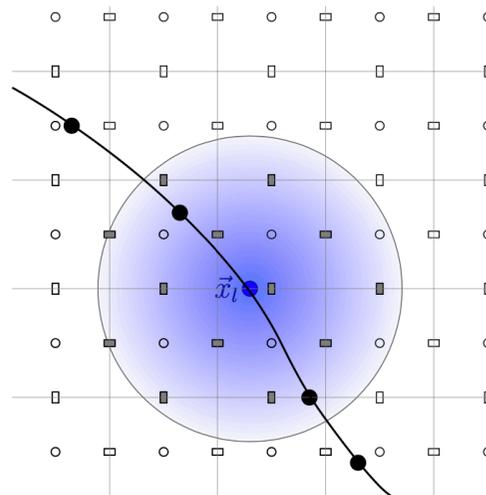
- Coupling net and fluid dynamics
 - Structure cannot be resolved in fluid domain
 - Hydrodynamic forces on net using screen force model (alternative to Morison equation)
 - Effect of net on fluid through additional source term in Navier-Stokes equations



screen force model

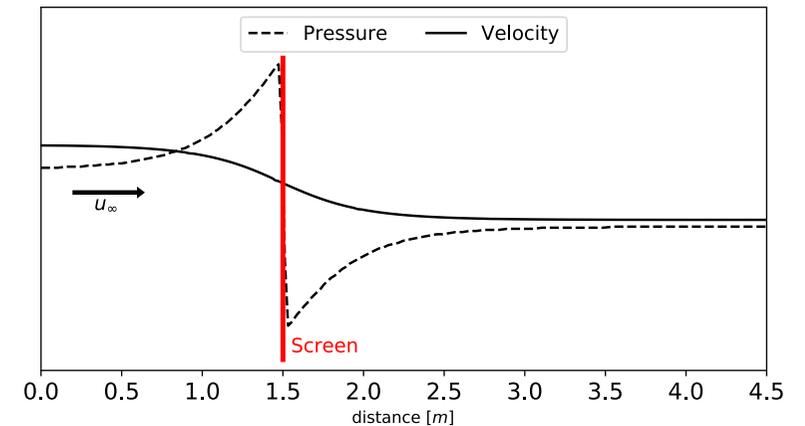
$$\vec{F}_D = \frac{\rho}{2} C_D A u_{rel}^2 \vec{n}_d,$$

$$\vec{F}_L = \frac{\rho}{2} C_L A u_{rel}^2 \vec{n}_l,$$



Lagrangian markers within a kernel D

$$\frac{\partial}{\partial x_i} \left(\frac{1}{\rho} \frac{\partial p^{(n+1)}}{\partial x_i} \right) = \frac{1}{\Delta t} \frac{\partial}{\partial x_i} \left(u_i^{(*)} - F_i \right),$$



resulting pressure jump at the net

Net Dynamics Model

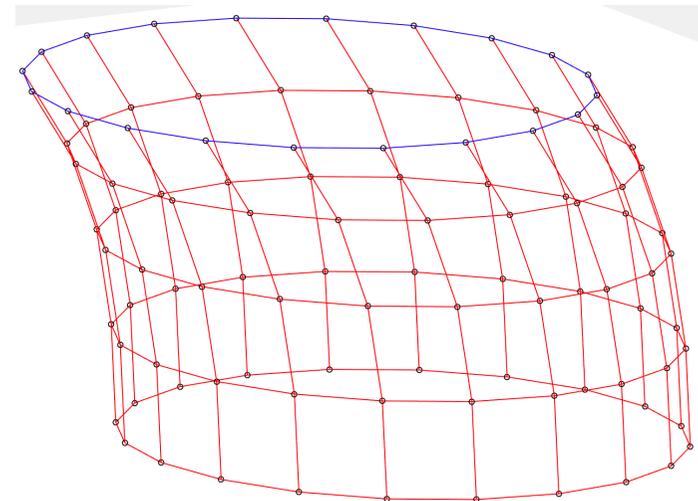
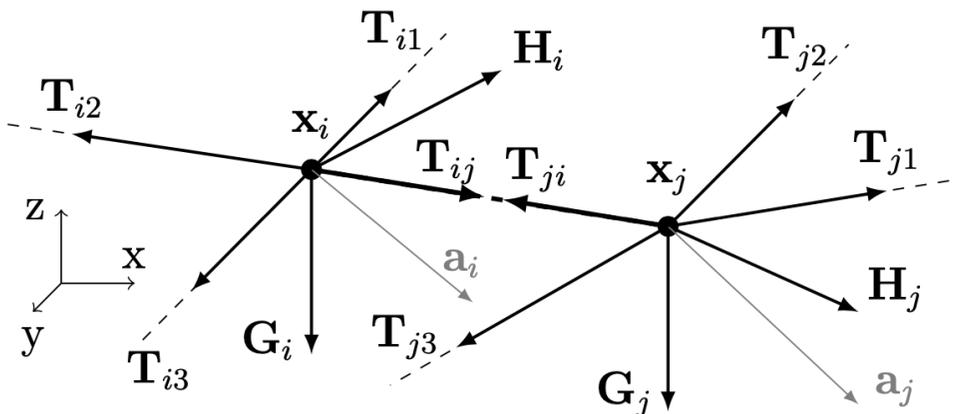
- **Challenges:**

- Non-linear material laws
- Large deformations
- Two distinct stress directions

$$m_i \mathbf{a}_i = \sum_{k=1}^{N_i} \mathbf{T}_{ik} + \mathbf{F}_i.$$

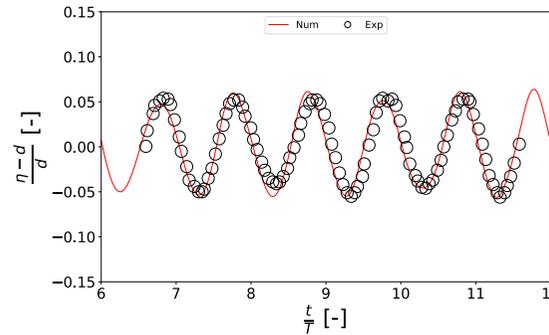
- **Solution:**

- finite number of mass points
- connected by non-linear elastic bars pointing in the principal directions of the meshes
- Solving dynamic force equilibrium (Newton's second law)
- Implicit method to keep physical connections automatically fulfilled

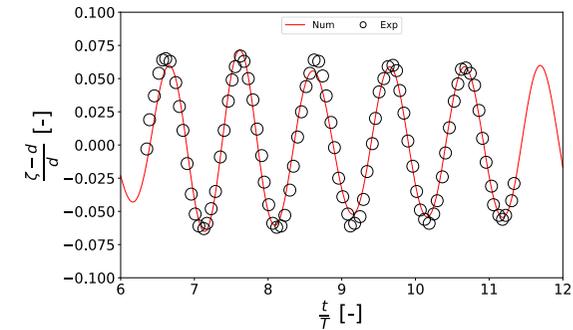


Floating Algorithm Validation

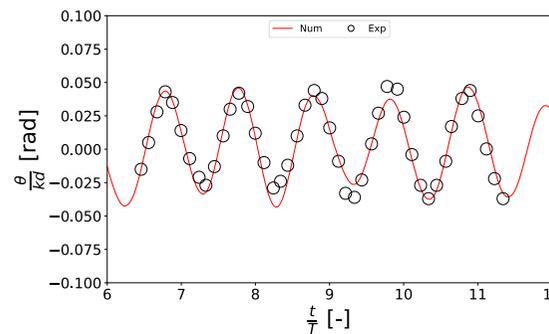
- $d = 0.4\text{m}$
- barge density = 500 kg/m^3
- $H = 0.04\text{m}$
- $T = 1.2\text{s}$



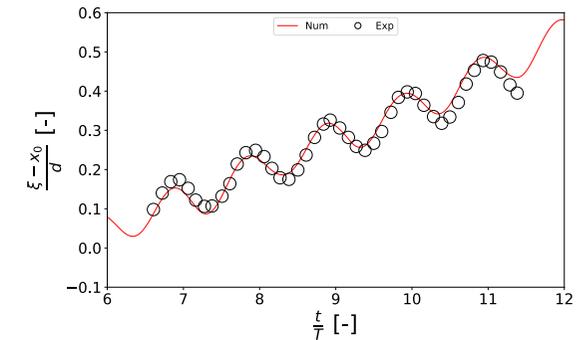
(a) Wave elevation over time at $x = 5.5\text{ m}$.



(b) Heave motion over time.



(c) Pitch motion over time.

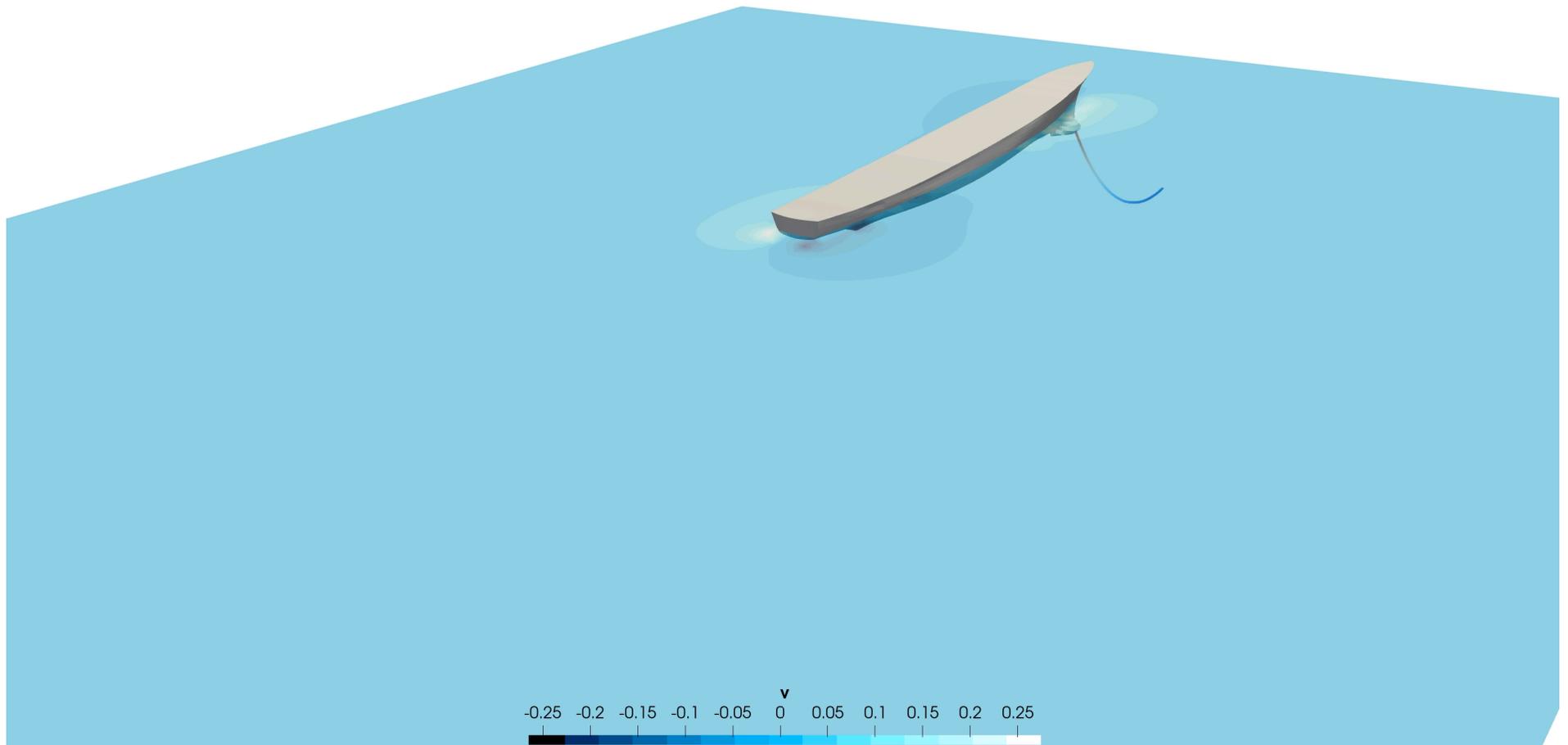


(d) Surge motion over time.

Figure 10: 3DOF motion of the two-dimensional barge over time. Comparison of numerical and experimental results for $\Delta x = 0.01\text{ m}$ and $\text{CFL} = 0.1$.

Mooring Models

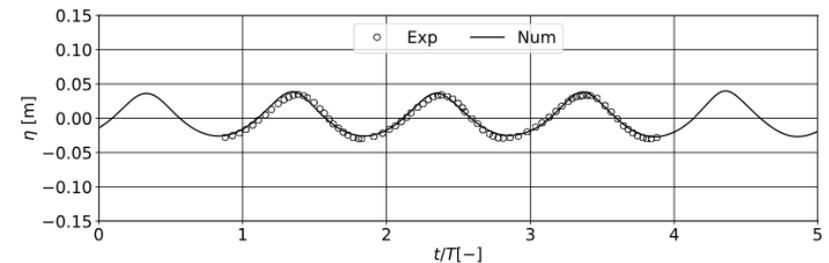
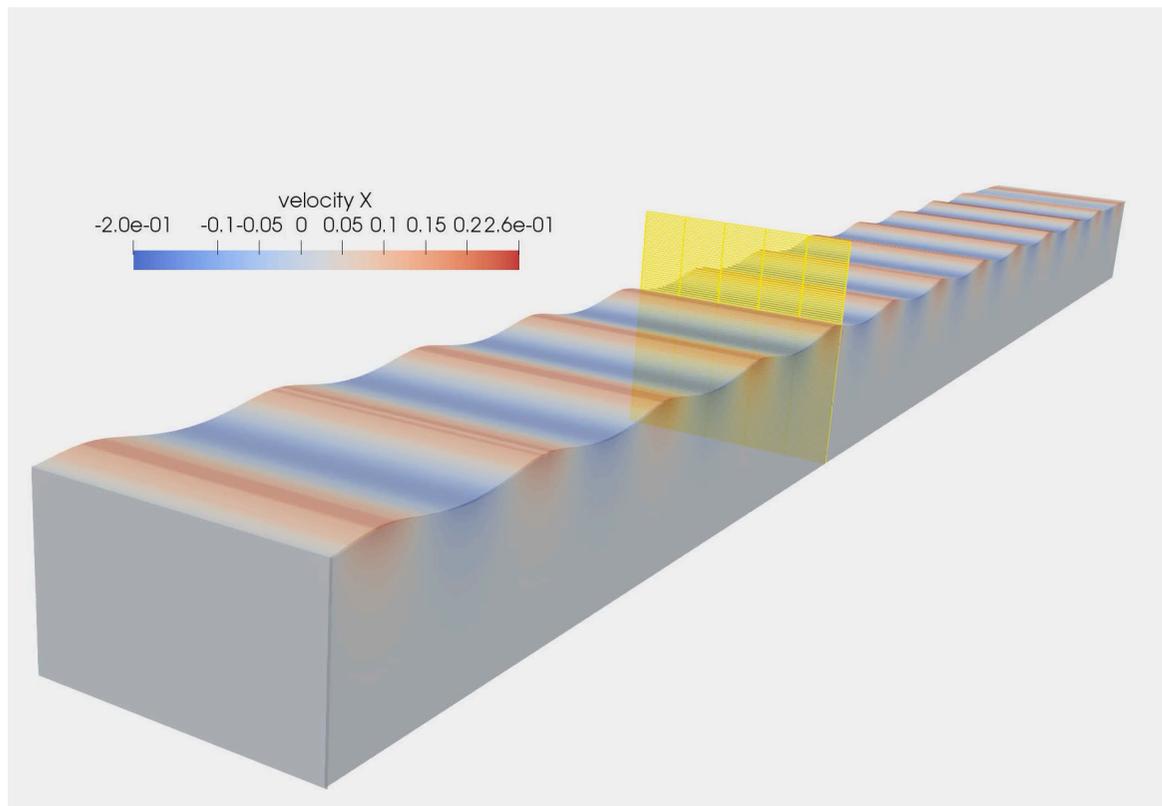
- Quasi-static approach = Robustness



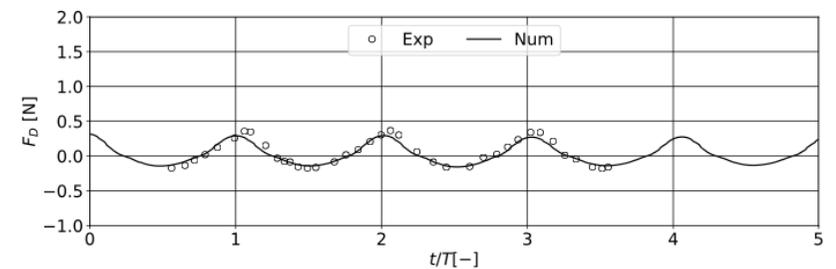
Net Model Validation: Waves

- ▶ Fixed net panels with $S_n = 0.095 - 0.288$ in regular waves
- ▶ Wave heights $H = 0.045 \text{ m} - 0.167 \text{ m}$.
- ▶ Wave frequencies $f = 1.0 \text{ Hz} - 1.42 \text{ Hz}$.
- ▶ 5th-order Stokes waves.

P.F. Lader et al. "Experimental Investigation of Wave Forces on Net Structures". In: *Applied Ocean Research* 29 (3) (2007), 112–127.



(a) Surface elevation at the wave gage.

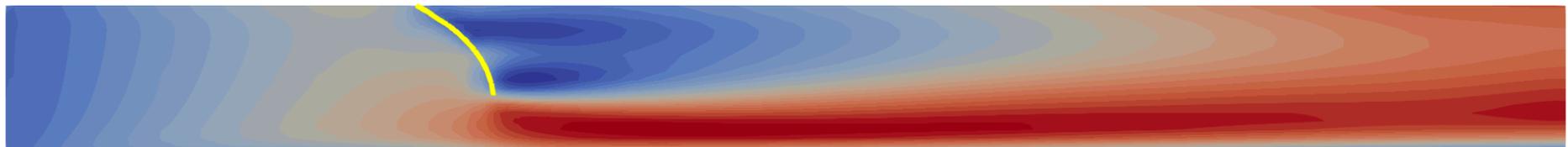
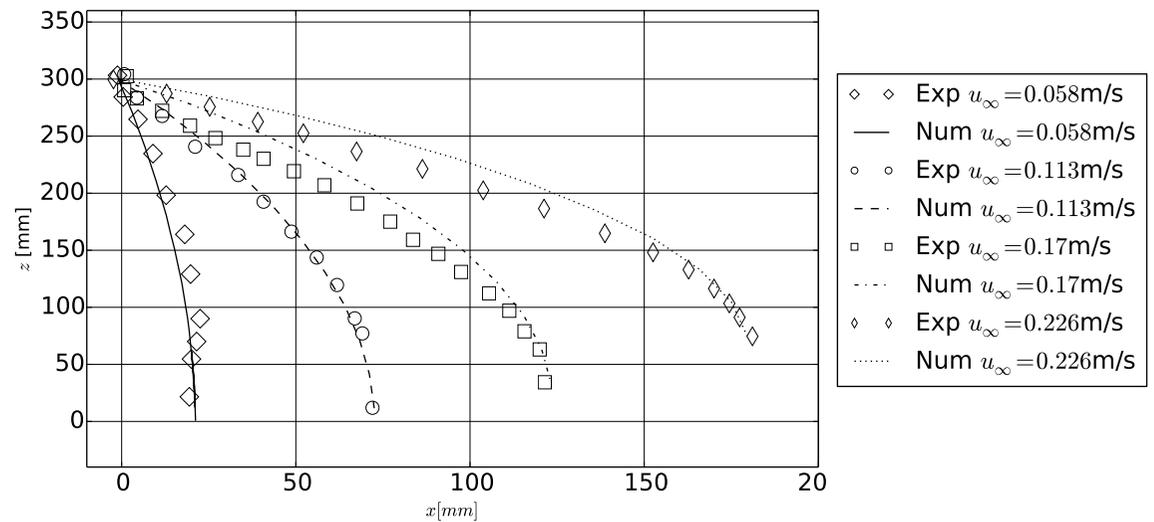
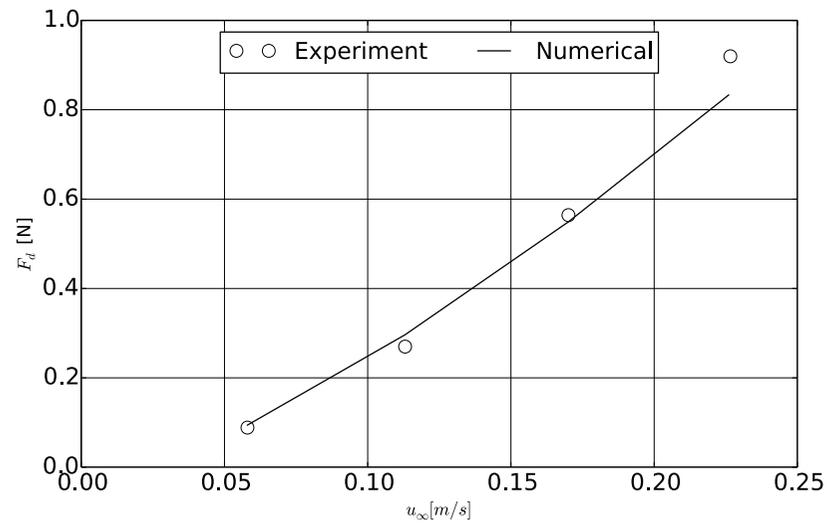


(b) Drag force for net case 1.

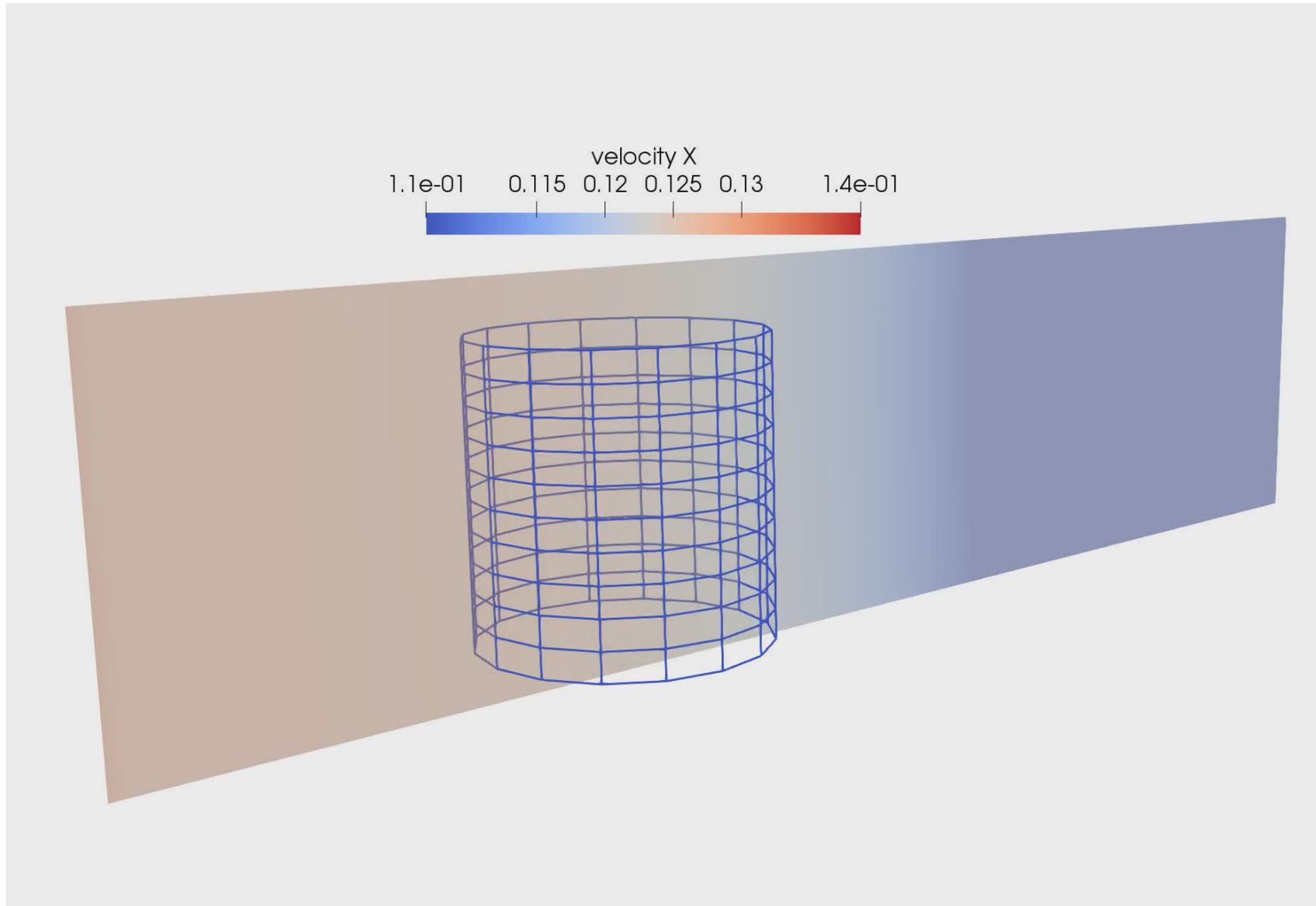
Net Dynamics Model Validation

- Validation for moving net wall in current

C.-W. Bi et al. "Numerical simulation of the interaction between flow and flexible nets".
In: *J. Fluids Struct.* 45 (2014), 180–201.



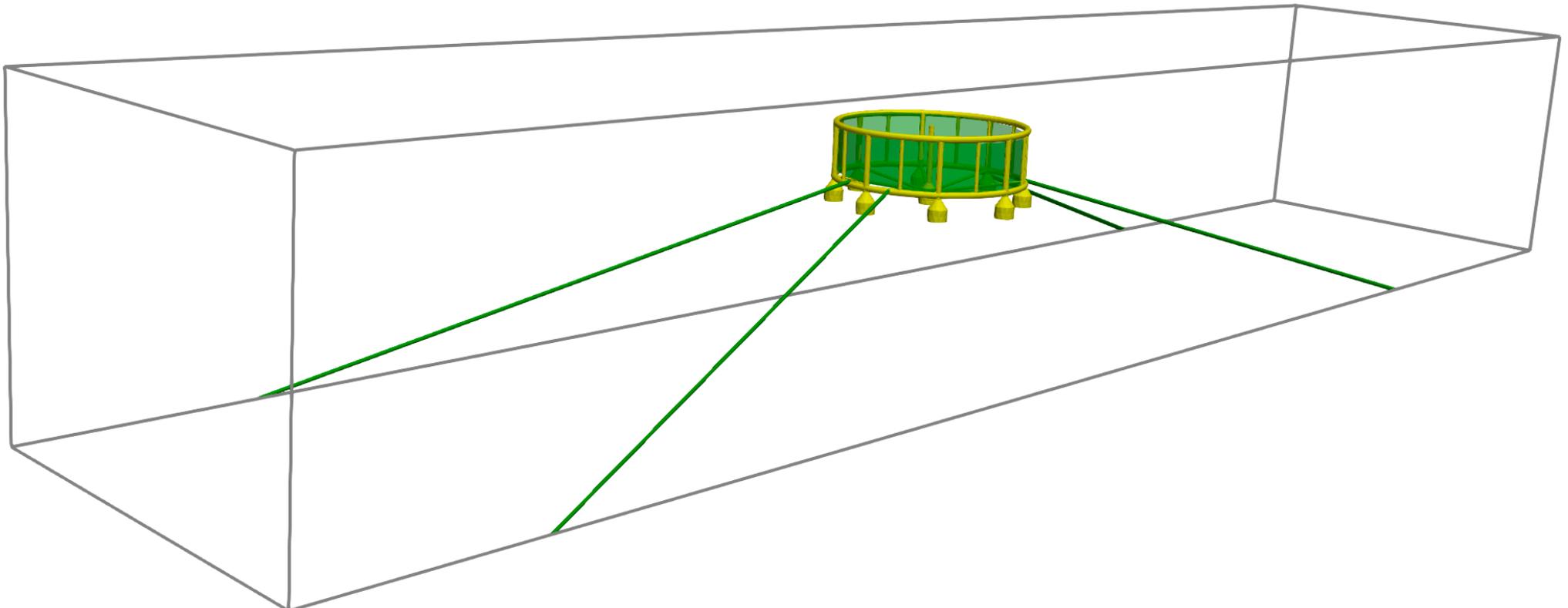
Net Model



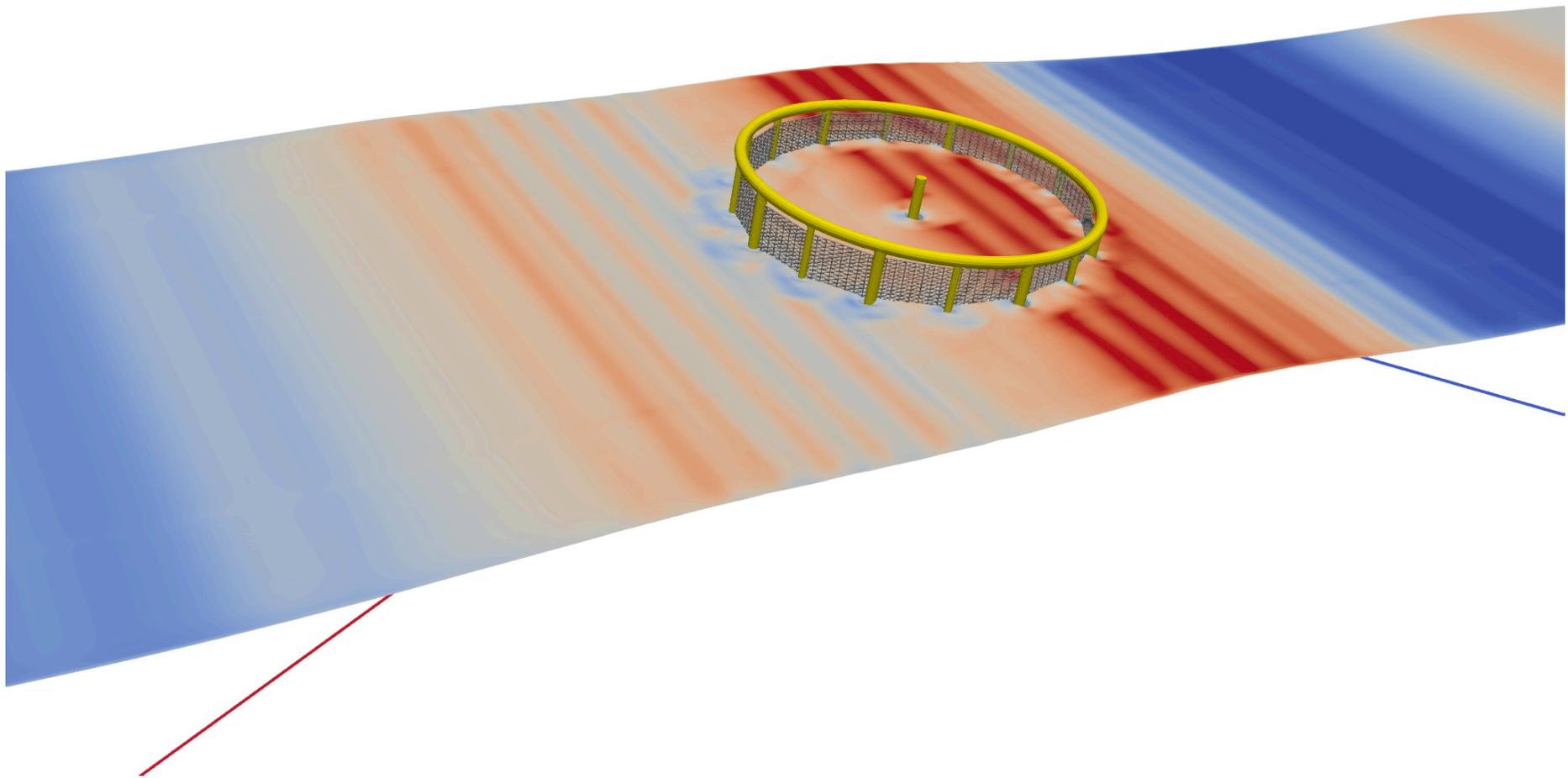
Application to Open Ocean Aquaculture structures

- ▶ Circular structure with $D = 1$ m adapted from Zhao et al.
- ▶ 9 pontoons with columns on top connected with pipes.
- ▶ Uniform mass distribution assumed.
- ▶ Rigid net system with solidity 0.145.
- ▶ Mooring system: 4 linear springs with pretension.
- ▶ Convergence test for heave and pitch decay $\rightarrow \Delta x = 8$ mm around structure.
- ▶ Regular waves with $H = 0.06$ m and 0.1 m and $T = 1.0$ s, 1.2 s, 1.4 s.
- ▶ Jonswap spectra with $H_s = 0.1$ m and $T_p = 0.5$ s – 3.5 s.
- ▶ Response amplitude operators from power spectra using discrete FFT.

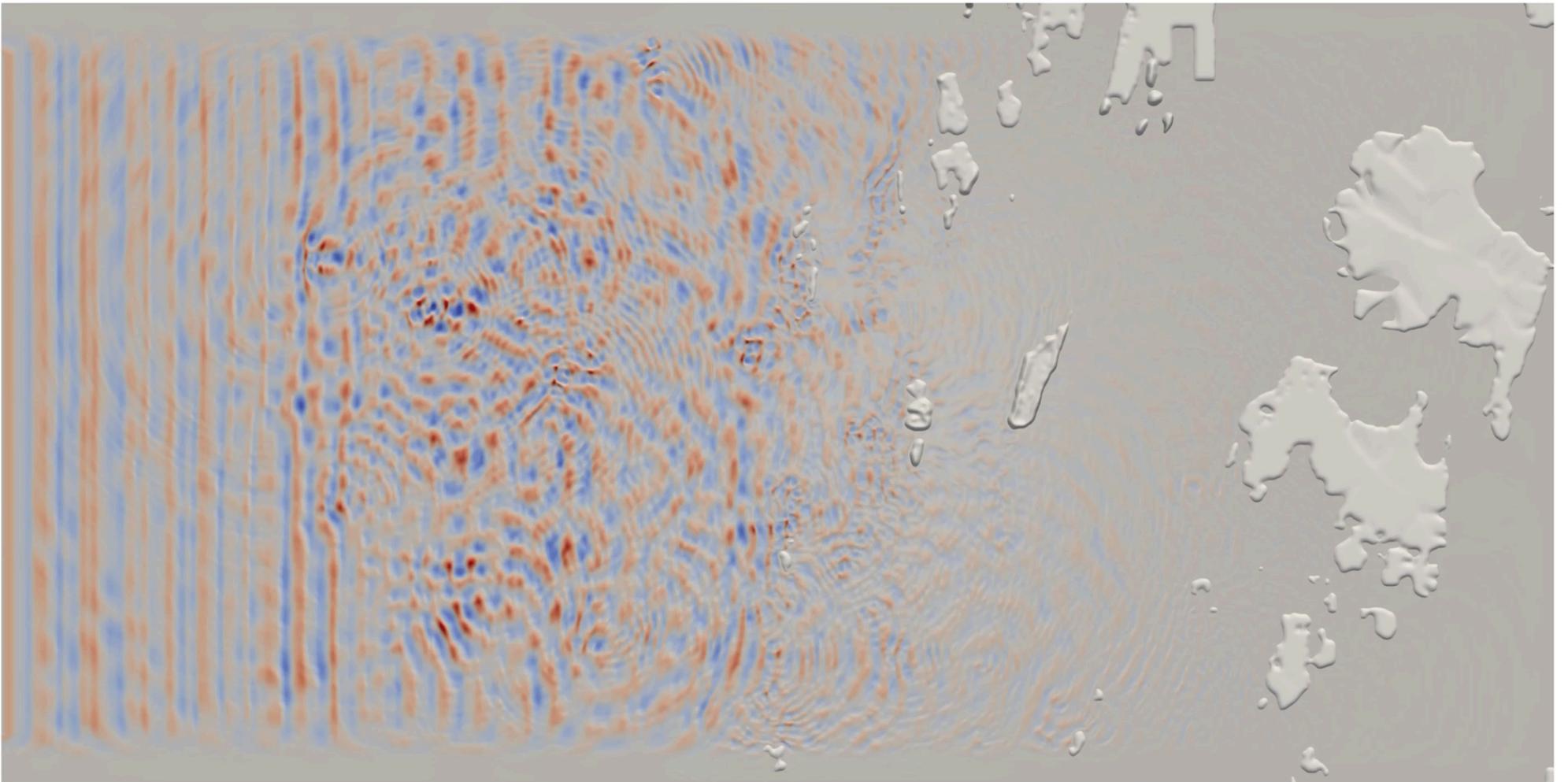
Y. Zhao et al. "Experimental Investigations on Hydrodynamic Responses of a Semi-Submersible Offshore Fish Farm in Waves". In: *Journal of Marine Science and Engineering* 7 (2019). DOI: 10.3390/jmse7070238.



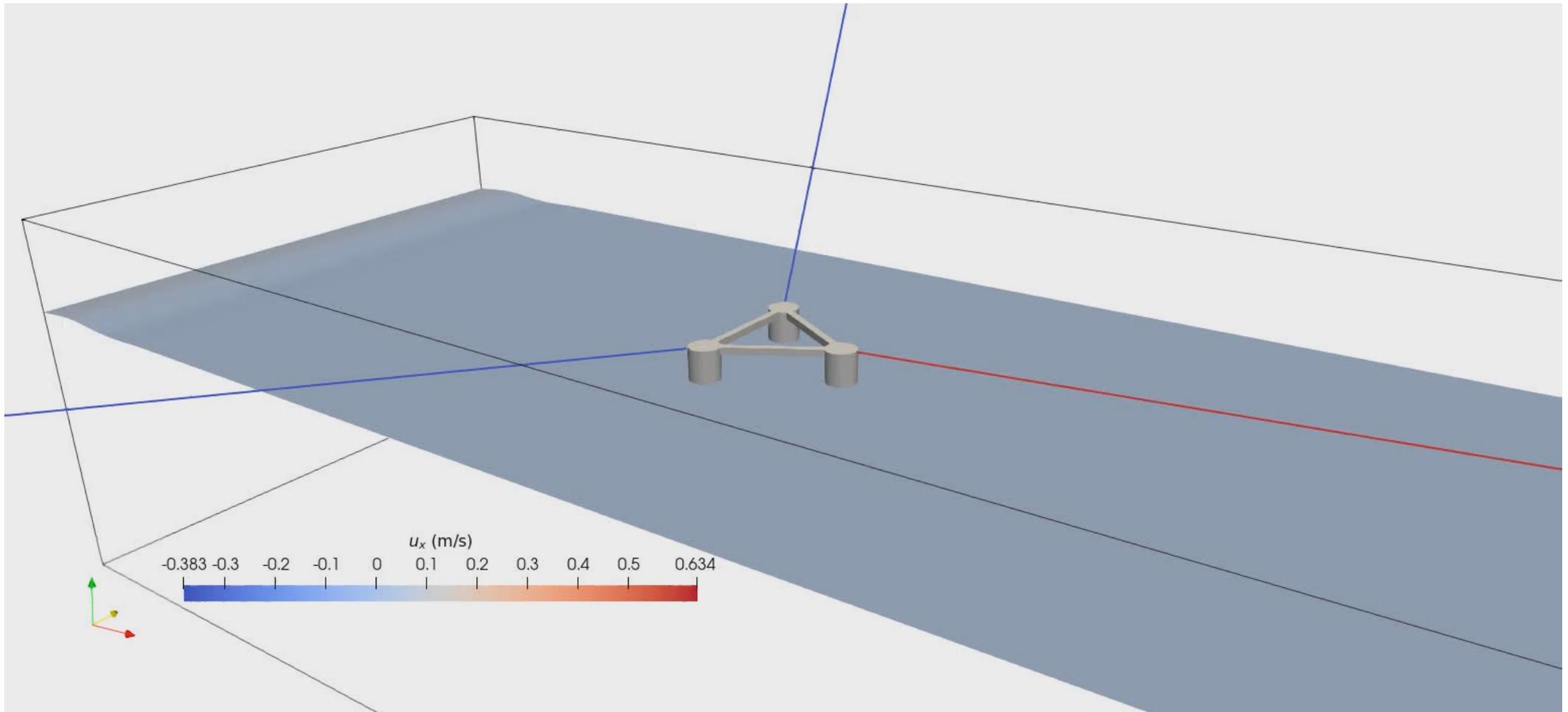
Application to Open Ocean Aquaculture structures



Flatøya Aquaculture Site



WINDMOOR floating offshore wind



Vegetation in a flow field

